

**DORNIER**

Dornier Medizintechnik GmbH - München

FACSIMILE TRANSMISSION LEAD SHEET

from: DORNIER MEDIZINTECHNIK GMBH  
POB 1128  
D-8034 Germering

Dept.: HT 20Name : Steigerto: Mr. JversonDate: 15. 10. 1987

No: \_\_\_\_\_

Number of sheets including lead sheet:

33Sheet : 33

We transmit and receive with Model ITT 3534  
on group III and group II mode.

**BEST AVAILABLE COPY**

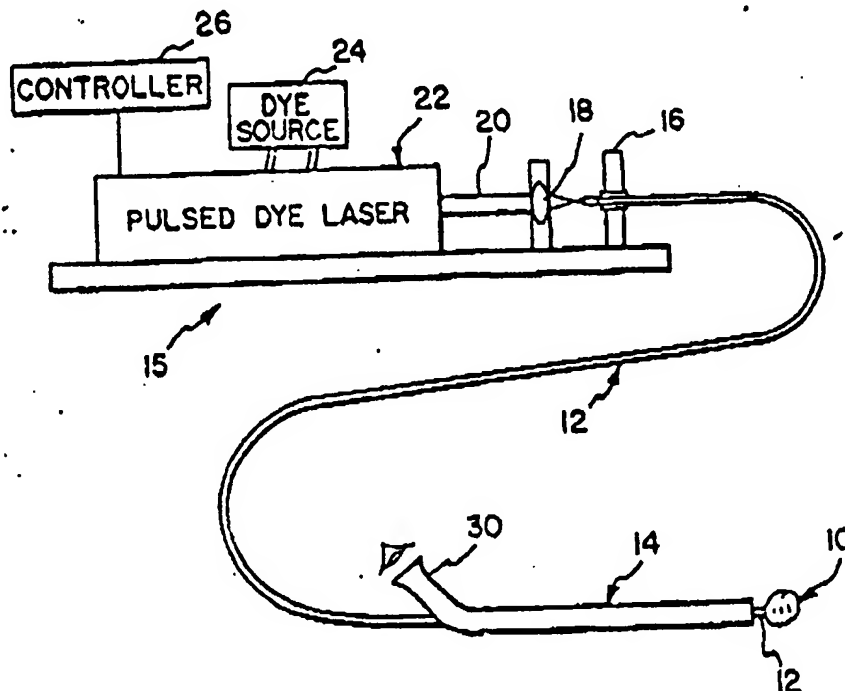
PCT

WORLD INTELLECTUAL PROPERTY ORGANIZATION  
International BureauSAMUELSON  
Patentabl. DORNIER  
S 44L

## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification <sup>4</sup> : <b>A61B 17/00</b>	<b>A1</b>	(11) International Publication Number: <b>WO 86/ 06269</b>
		(43) International Publication Date: 6 November 1986 (06.11.86)
<p>(21) International Application Number: <b>PCT/US86/00886</b></p> <p>(22) International Filing Date: <b>23 April 1986 (23.04.86)</b></p> <p>(31) Priority Application Number: <b>726,472</b></p> <p>(32) Priority Date: <b>24 April 1985 (24.04.85)</b></p> <p>(33) Priority Country: <b>US</b></p> <p>(71) Applicants: <b>CANDELA CORPORATION [US/US]: 19 Strathmore Road, Natick, MA 01760 (US). THE GENERAL HOSPITAL CORPORATION [US/US]: 55 Fruit Street, Boston, MA 02210 (US).</b></p> <p>(72) Inventors: <b>FURUMOTO, Horace : 14 Woodridge Road, Wellesley, MA 02181 (US). WATSON, Graham : 60 Lysias Road, London SW12 8BT (GB).</b></p> <p>(74) Agents: <b>SMITH, James, M. et al.: Hamilton, Brook, Smith and Reynolds, Two Militia Drive, Lexington, MA 02173 (US).</b></p>		<p>(81) Designated States: <b>AT, AT (European patent), AU, BE (European patent), BR, CH, CH (European patent), DE, DE (European patent), FR (European patent), GB, GB (European patent), IT (European patent), JP, KR, LU, LU (European patent), NL, NL (European patent), SE, SE (European patent).</b></p> <p><b>Published</b> <i>With International search report. Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</i></p>

(54) Title: USE OF LASERS TO BREAK DOWN OBJECTS



(57) Abstract

Calculi, stones, calcified tissue and other material are broken down for removal from within a body using laser pulses that are delivered via an optical fiber and have a wavelength, intensity, energy per pulse and pulse duration selected to break down the object into smaller particles without delivering energy sufficient to cause damage to other tissue.

-1-

USE OF LASERS TO BREAK DOWN OBJECTSBackground

05 This invention relates to using a laser beam delivered via an optical fiber to break down a calculus, stone or calcified tissue or other material for removal from within the human body.

10 Frequently such calculi, stones, or calcified tissue are located in positions which can be reached using only small diameter endoscopes and the optical fiber must be fine enough to pass via the endoscope. The stones are typically in close proximity to healthy tissue.

Summary of the Invention

15 The general feature of the invention is in delivering via the optical fiber laser pulses having a wavelength, energy, intensity and pulse duration which will break down the calculus, stone, calcified tissue or other material into smaller particles without delivering energy sufficient to cause damage to other tissue in the same vicinity.

20 The material to be removed from the body is illuminated in a localized region with a pulsed laser. By surrounding the material with liquid and illuminating the localized region with light above a threshold intensity level, a shock wave can be generated from the localized region. It is believed that the shock wave fragments the materials beyond the localized region even though heating is limited to the localized region.

-2-

05 Thus, the stone is safely and relatively quickly broken down into easily removed sand-like particles, without melting. Thermal damage to surrounding tissue is limited. The stone and the particles are not propelled into the surrounding tissue. Degradation of the optical fiber by the laser beam is limited. The fiber can be sufficiently small in diameter to be useful with small diameter endoscopes.

The preferred embodiments include the following features. The pulses are at wavelengths corresponding to wavelengths for which the object has a relatively shallow depth of penetration. Preferably wavelengths between 350 and 550 nanometers are used for urinary calculi (most preferably 251, 504, or 450 nanometers). The laser is preferably of the pulsed dye type for relatively long pulse durations but may be of other types. The pulses have durations of at least 10 nanoseconds (preferably between .05 and 2 microseconds), and the pulse energy is no greater than .200 joules, preferably between .005 and .200 joules. The fiber is flexible and has a core diameter no greater than 1000 microns, preferably between 60 and 600 microns, and more specifically 200 microns. The distal end of the fiber is in contact with the object (a stone) and the interface between them is surrounded by fluid. The laser pulses are applied in brief bursts, preferably greater than 10 hertz, and remaining fragments are broken down by one-shot pulses.

WO 86/06269

PCT/US86/00886

-3-

Other advantage and features of the invention will become apparent from the following description of the preferred embodiment, and from the claims.

#### Drawings

05 Fig. 1 is a diagram of a system for breaking down unwanted objects or tissue.

Fig. 2 is a family of curves showing fragmentation thresholds versus pulse energy for different pulse durations.

10 Fig. 3 is a family of curves indicative of fragmentation threshold pulse energy versus wavelength for different types of stones.

Fig. 4 is a family of curves indicative of fragmentation threshold pulse energy versus fiber area for different types of stones.

15 Fig. 5 is a curve indicative of fragmentation threshold pulse energy versus pulse repetition rate.

Fig. 6 is a diagram of pulse timing.

#### Description of the Preferred Embodiments

20 Referring to Fig. 1, a urinary calculus (stone) 10 to be removed from within a human body is contacted by the cleaved distal face of a flexible quartz silica optical fiber 12 (Superguide series available from Fiberguide Industries) having a core diameter in the range of 60 to 400 microns. Fiber 25 12 passes through a ureteroscope 14 and extends to a laser source 15, where the proximal face of fiber 12 is held in a fiber mount 16 (Model FP2 available from Newport Corporation). The proximal face of

-4-

fiber 12 is exposed to receive, via a convergent lens 18, (of appropriate focal length for the fiber), a beam 20 from a linear flash lamp pumped pulsed dye laser 22. Laser 22 is connected to a source 24 of dye of a selected wavelength characteristic. Laser 22 is also connected to a controller 26 which includes a control panel to permit the user to activate and deactivate the laser and to vary the pulse energy and pulse repetition rate of the laser beam. Laser 22 and controller 26 are available from Candela Corporation, Natick, Massachusetts.

Ureteroscope 14 includes an eyepiece 30 through which the user can observe the stone and the distal end of the fiber, as well as a light source (not shown) to illuminate the distal end for viewing and an irrigation lumen to deliver an irrigant to the distal end.

The wavelength at which the laser will be operated (and hence the dye to be used) is chosen in part on the basis of the percentage transmission characteristics of the stone material. For example, the percentage transmission of calcium phosphate and calcium oxalate stone materials for different wavelengths was measured experimentally (by conventional spectroscopy) on sections of dry stones which were sanded to form progressively thinner wafers. The resulting graph of the log of the percentage transmission against thickness was linear indicating the following  $1/e$  depths of penetration for different wavelengths.

WO 86/06269

PCT/US86/00886

-5-

<u>1/e Depth of Penetration (mm)</u>			
<u>Wavelength (nm)</u>	<u>Calcium Phosphate</u>	<u>Calcium Oxalate</u>	
1064	2.16 + 0.8	3.58 + 0.85	
577	0.81 + 0.2	0.50 + 0.1	
504	0.54 + 0.05	0.30 + 0.2	
450	0.42 + 0.05	0.24 + 0.05	
308	0.25 + 0.03	0.18 + 0.1	

10 The penetration depth decreases with shorter wave-  
 lengths. The smallest penetration depth is the most  
 desirable from the point of view of enabling a low  
 energy threshold to accomplish fragmentation,  
 producing small-size fragments, and limiting the  
 propulsion of fragments into surrounding tissue.  
 Very short wavelengths (shorter than 350 nm) in the  
 15 ultraviolet range (for example 308 nm), however, are  
 known to be mutagenic and are difficult to deliver  
 via the optical fiber and therefore are avoided.  
 Wavelengths in the range 450 to 550 nanometers are  
 preferred. Dyes are available which operate at the  
 20 450 nm (blue) and 504 nm (green) wavelengths. The  
 450 nm dye fades fairly rapidly. Where the cost of  
 the dye is an issue, the best choice is the 504 nm  
 dye.

25 The duration of each pulse delivered by the  
 laser is chosen to minimize the energy delivered to  
 the stone while still accomplishing fragmentation  
 (i.e., the breaking down of the stone into smaller  
 particles). Referring to Fig. 2, the threshold  
 energy in millijoules per pulse required to initiate

WO 86/06269

PCT/US86/00886

-6-

fragmentation of an oxalate stone for a given pulse duration at 577 nm using a 600 micron optical fiber was determined experimentally by measuring an acoustic signal in the stone resulting from the pulse. The acoustic signal was measured electronically in millivolt units. Dashed line 30<sup>2</sup> represents the acoustic level (nominally 400 millivolts) which corresponds to the initiation of fragmentation in a stone. Each curve represents, for a given pulse duration, the variation of acoustic signal with energy per pulse. The point at which each curve crosses line 30<sup>2</sup> is the threshold pulse energy level at which fragmentation will occur. The threshold energy level decreases with decreasing pulse duration. Because lower energy pulses are less likely to cause thermal damage or to propel the stone or the broken off particles into surrounding tissue, pulse durations of less than 10 microseconds, preferably between .05 and 2.0 microseconds, are used.

Referring to Fig. 3, the pulse energy threshold for causing an acoustic signal at a given level (25 millivolts) was determined for three different stone types at three different wavelengths, further confirming the desirability of using shorter wavelengths regardless of the stone material.

Referring to Fig. 4, the relationship between cross-sectional area of fiber 12 and the threshold pulse energy required to cause an acoustic signal at the 25 mv level was determined for three different stone materials. In all cases the threshold pulse



WO 86/06269

PCT/US86/00886

-7-

energy decreases linearly with fiber area. Different fiber sizes have been used: 1000, 600, 400, 200, 100 and 60 microns.

05 The pulse repetition rate may also be chosen to reduce the threshold pulse energy at which fragmentation is expected to occur. Referring to Fig. 5, the energy required to produce the 25 mv acoustic signal decreased with increasing pulse repetition rate. Furthermore, at higher repetition rates, the  
10 fragmentation proceeds more rapidly. At higher repetition rates, however, the dye is depleted faster and the optical fiber is less capable of passing the energy to the stone. A maximum practical rate is not much greater than 100 Hertz and the  
15 optimum rate is about 20 Hertz.

It can be shown experimentally that above the energy pulse threshold, the average weight of fragments yielded per pulse increased sharply and that laminated oxalate stones have a substantially  
20 lower fragmentation threshold than do homogeneous oxalate stones. Thus the pulse energy can be varied to break down different stones.

#### Operation

25 In operation, after inserting the ureteroscope 14 to reach the site at which the stone 10 is located, the distal end of the fiber 12 is inserted through the ureteroscope and oriented by sight, so that the distal face of the fiber is in contact with the stone 10. The site is irrigated via a lumen in  
30 the ureteroscope so that the stone is surrounded by

WO 86/06269

PCT/US86/00886

-8-

liquid. The laser is set at a wavelength between 450 and 550 nanometers by selecting an appropriate dye. The pulsed dye laser controller 22 is adjusted to set the pulse energy and pulse repetition rate. 05 The laser pulse energy is initially set at a value which is lower than the threshold fragmentation level and then increased until the desired fragmentation effect has been attained. Preferably the pulsed dye laser is operated at about 30 milli- 10 joules per pulse for a 200 micron fiber and about 100-150 millijoules per pulse for a 600 micron fiber, and in no event more than about 200 millijoules. The pulse repetition rate is set between 10 and 50 Hertz.

15 Referring to Fig. 6, the laser 22 is activated for a brief burst, for example for a period of a second or a fraction of a second (identified as 40 in Fig. 6). The laser pulse duration 42 is typically between 0.1 and 2.0 microseconds. The period 20 of the pulse repetition is identified as 44 on Fig. 6. During activation period 40, a portion of the stone breaks down into a combination of vapor and sand-like particles small enough to be easily removed.

25 The distal face of the fiber is then reoriented (during a period identified as 45 in Fig. 6) to be once again in contact with the stone. Then the laser is again activated briefly for a burst period 46, to cause another portion of the stone to break 30 down. The process is repeated until the entire stone has been broken down. Any fragments which

WO 86/06269

PCT/US86/00886

-9-

need to be broken down further can then be broken down by touching them with the distal end of the fiber and applying a single shot laser pulse.

05 The stone is safely and relatively quickly broken down into easily removed sand-like particles, without melting. Thermal damage to surrounding tissue is limited. The stone and particles are not propelled into the surrounding tissue. Degradation of the optical fiber by the laser beam is limited.  
10 The fiber can be sufficiently small in diameter to be useful with small diameter endoscopes.

Other embodiments are within the following claims. For example, although less desirable, laser 22 can be an excimer laser tuned to a particular  
15 wavelength by a selected gas mixture. The wavelength is chosen to be as short as possible while still permitting the pulses to be delivered via the optical fiber. Preferably the gas mixture is xenon-fluoride providing a wavelength of 351 nm.  
20 The resulting pulses have very shallow penetration into the stone and operate to break the stone into extremely fine particles and vapor. Progress through the stone is slower per pulse than for the pulsed dye laser, but this is offset by higher pulse  
25 repetition rates which are possible with the excimer laser. The pulse durations typical of excimer lasers are 10 nanoseconds but can be lengthened by various techniques to 80 or more nanoseconds. Such pulse durations make the pulses somewhat more  
30 difficult to deliver via the optical fiber than the pulsed dye laser pulses.

WO 86/06269

PCT/US86/00886

-10-

Using the excimer laser on an oxalate calculus via a 1000 micron fiber at 351 nm, a repetition rate of 200 Hertz, and a pulse energy of 30 millijoules (energy density of 1.6 joules/cm<sup>2</sup>), produced an  
05 average yield of fragments per pulse of 10 micrograms. By comparison, using the pulsed dye laser at 450 nm and a pulse energy of 20 joules/cm<sup>2</sup> via a 600 micron fiber generated 100 micrograms of fragments per pulse. Using the pulsed dye laser at 504 nm at  
10 a pulse energy of 25 joules/cm<sup>2</sup> via a 600 micron fiber yielded 1 milligram per pulse.

The product of breaking down the stone is about 90% vapor for the excimer laser and 10% for the pulsed dye laser.

15 In other embodiments, gallstones or arterial plaque may be broken down by a pulsed dye laser at 450 nm, and any appropriate technique for reaching the stone with the distal end of the fiber may be used.

20 The following describes observations made in the process of breaking down calculus, stone and calcified tissue using a laser.

1. Laser radiation is absorbed by the target material at wavelengths characteristic of its  
25 absorption spectra. Laser light of shorter wavelengths is better for white or translucent material.

-11-

- 05 2. The laser intensity must be greater than a certain level before a significant effect is observed. The intensity is proportional to the energy delivered and inversely proportional to the pulse duration of the laser, and the distal end of the fiber must touch or be in close proximity to the target for maximum effect. However, a fiber is not necessary inasmuch as the same effect can be obtained by focusing the laser beam on the target so that the intensity threshold is reached.
- 10
- 15 3. When the threshold for breakdown is reached, a loud acoustic signal is heard. The target material must be completely immersed in liquid for maximum breakdown. A wetted target or a target slightly below the surface of the liquid (2 or 3 mm) will give a loud acoustic signal but will not readily break down the target.

20 It is believed that the fragmentation process is as follows:

1. The laser radiation is first absorbed by the target. For white or translucent material, shorter wavelengths are preferred.
- 25 2. A minimum laser threshold intensity (power per unit area) is necessary to vaporize, heat and ionize the target.

-12-

3. The laser energy is confined in a small volume by a surrounding liquid. Increasing the energy density as more laser light is absorbed increases the pressure in the volume to several hundred kilobars. At such pressures, shock waves with average velocities over 0.5 mm per microsecond can be formed. "Laser Induced High Pressure Shock Waves in Water", C.E. Bell and J.A. Landt, Applied Physics Letters 10, 46 (1966) and "Intense Ruby Laser Induced Acoustic Impulses", E.F. Carame, C.E. Moeller and N.A. Clark, Jrn of Acoustical Soc of America 40, 1463 (1966).

4. The spherical shock wave is propagated into the calculus, stone or calcified tissue to break it down. The liquid is necessary to confine the interaction volume so that a high pressure shock is generated. The liquid also helps to couple the shock wave into the target. If the target is only wetted or submerged slightly, the interaction volume expands so that only a moderate to weak shock is generated which will not break down the target.

There are several considerations in the optimization of the use of lasers to break down objects for removal from within the body. They are energy per pulse, intensity (power density), pulse duration, repetition rate, color, fiber size, and fiber damage level. These considerations are not

-13-

independent of each other. In addition, treatment time should be shortened whenever possible and risk of damage to living tissue in the body should be minimized.

- 05 1. Energy per pulse. Energy per pulse should be as large as possible to maximize the amount of material to be broken down in the shortest period of time.
- 10 2. Fiber size. Small fibers are preferred because they are more flexible and because endoscopes or catheters composing the delivery systems can be made smaller. Fibers over 600 microns in diameter are too large, while fibers smaller than 60 microns will not be able to transmit much total power or energy, thereby increasing treatment time. One to two hundred micron fibers are considered optimum.
- 15 3. Intensity. The laser intensity out of the fiber must be high enough to form a shockwave at the target. This effect has a threshold which has been shown to be 5 megawatts per square centimeter. An intensity of at least 10 megawatts per square centimeter is preferred. The area of the spot is determined by the fiber cross section. The highest intensity occurs when the fiber touches the target and intensity is quickly reduced as the fiber is withdrawn from contact. A lens system to focus the light from the fiber on to the target to obtain the desired intensity is conceivable but difficult to reduce to practice. Furthermore, the shock generated erodes the fiber tip. This is not too serious
- 20 25 30

 $5 \text{ MW/cm}^2$

WO 86/06269

PCT/US86/00886

-14-

for the distal surface of the cleaved fiber tip but is a serious effect for a lens unless the lens is far removed from the focus.

4. Pulse duration. Total power for a given energy can be increased by reducing pulse duration. Typical Q switched, excimer or nitrogen lasers will have pulse durations in the order of 1 to 20 nsec. The damage intensity for quartz fiber is about 300 to 400 megawatts per square cm. A 400 micron fiber will transmit approximately 10 mj in a 20 nsec pulse at the damage level provided that the laser uniformly illuminates the fiber. However, the laser beam must be focused into the fiber and peak intensity spots will limit the total energy to a few millijoules. Higher energy throughput is desired for rapid treatment.

Longer pulses of at least .05 <sup>50 nsec</sup> microseconds, and preferably greater than the .1 <sup>100 nsec</sup> microseconds available with dye lasers, allow more energy to be transmitted for a given fiber size. However, too long a pulse will allow the interaction volume to expand and the shock to dissipate. For high pressure shocks in liquids, a pulse duration 2 microseconds or less is desired.

5. Repetition rate. The higher the setting of the repetition rate, the faster is the treatment. However, single shot capacity is also necessary to further fragment small broken off particles.



WO 86/06269

PCT/US86/00886

-15-

Table I sets forth the optimized operating ranges for various treatments. A flashlamp excited dye laser can be designed to perform at the optimum conditions for each of the listed treatments.

- 05        A less desirable embodiment is the use of an excimer, gold or copper vapor, frequency doubled repetitively switched YAG or a nitrogen laser for laser 22. These lasers have higher peak output powers and shorter pulse durations than a flashlamp
- 10        excited dye laser and the fiber damage threshold of  $400 \text{ MW/cm}^2$  is reached at relatively low energy. The higher intensity requires the use of larger diameter fiber to prevent damage to the fiber and allows for even larger diameter fibers while still providing
- 15        the threshold intensity. The material is not fragmented substantially beyond the illuminated region. The fragments which are generated are much finer than those obtained with the long pulse laser. The amount of material removed per pulse for a given
- 20        fiber size is much lower for the high peak power laser than for the pulsed dye laser, so high repetition rates should be used.

Table II of optimized operating ranges has been assembled for the high peak power lasers.

WO 86/06269

PCT/US86/00886

-16-

TABLE I

## Optimized Operating Range for a Pulsed Laser

	Urinary Calculi	Callstones	Calcified Tissue
Fiber Diameter (low)	60 microns	60 microns	60 microns
Fiber Diameter (high)	600 microns	600 microns	600 microns
Fiber Diameter (optimum)	200 microns	200 microns	200 microns
Energy/Pulse (low)	5 mj	5 mj	5 mj
Energy/Pulse (high)	100 mj	100 mj	200 mj
Pulse Duration	.05 to 2 $\mu$ sec	.05 to 2 $\mu$ sec	.05 to 2 $\mu$ sec
Rep Rate (single shot)	Desireable	Desireable	Desireable
Rep Rate (optimum)	20 Hz	20 Hz	20 Hz
Intensity (low)	5 MW/cm <sup>2</sup>	5 MW/cm <sup>2</sup>	5 MW/cm <sup>2</sup>
Intensity (high)	400 MW/cm <sup>2</sup>	400 MW/cm <sup>2</sup>	400 MW/cm <sup>2</sup>

WFO 86/06269

PCT/US86/00886

TABLE II

Operating Range for a Low Energy but High Peak Power Pulsed Laser

	Urinary Calculi	Gallstones	Calcified Tissue
Fiber Diameter (low)	200 microns	200 microns	200 microns
Fiber Diameter (high)	1000 microns	1000 microns	1000 microns
Fiber Diameter (optimum)	600 microns	600 microns	600 microns
Peak Power for 600 Micron fiber (high)	1 MW	1 MW	1 MW
Pulse Duration	prefer 50-100 nsec	prefer 50-100 nsec	prefer 50-100 nsec
Rep Rate	100 Hz	100 Hz	100 Hz
Intensity (low)	5 MW/cm <sup>2</sup>	5 MW/cm <sup>2</sup>	5 MW/cm <sup>2</sup>
Intensity (high)	400 MW/cm <sup>2</sup>	400 MW/cm <sup>2</sup>	400 MW/cm <sup>2</sup>

-18-

Claims

1. Apparatus adapted for use in breaking down material for removal from within a body characterised in that it comprises:  
05        means for surrounding the material with liquid; and  
         means for illuminating a localized region of the material with a pulsed laser at such wavelengths and with sufficient energy and  
10        intensity to cause in the operation of the apparatus fragmentation of the material without delivering energy sufficient to cause significant damage to other tissue in the vicinity of said material.
- 15    2. Apparatus as claimed in Claim 1, wherein the illuminating means is capable of generating a shockwave from the localized region to cause fragmentation of the material substantially beyond the localized region.
- 20    3. Apparatus as claimed in Claim 1, wherein the illuminating means comprises optical fiber through which the localized region is illuminated in the operation of the apparatus.

WO 86/06269

PCT/US86/00886

-19-

4. Apparatus as claimed in Claim 3, wherein the distal end of the optical fiber is adapted to be placed in contact with or very near to the localized region of the material.
- 05 5. Appartus as claimed in Claim 1, wherein the pulsed laser is a dye laser.
6. Apparatus as claimed in Claim 1, 2, 3, 4 or 5 wherein the pulsed laser is arranged for a pulse duration between .05 microsecond and 2  
10 microseconds.
7. Apparatus as claimed in Claim 6 wherein the pulsed laser is arranged for a pulse duration greater than .1 microsecond.
8. Apparatus as claimed in Claim 6 wherein the  
15 illuminating means is capable of delivering an intensity of the light at the localized region reaching the level of at least 5 megawatts per square centimeter.
9. Apparatus as claimed in Claim 6, wherein the  
20 pulsed laser is capable of delivering energy per pulse between 5 millijoules and 200 millijoules.

WO 86/06269

PCT/US86/00886

-20-

10. Apparatus as claimed in Claim 6, wherein the optical fiber has a diameter of between 60 microns and 600 microns.
- 05 11. Apparatus as claimed in Claim 6 wherein the pulsed laser is adapted to apply pulse bursts to the material to fragment the material and, thereafter, single pulses to individual fragments to further break up the material.
- 10 12. Apparatus as claimed in Claim 11 wherein the pulsed laser is capable of a repetition rate of the pulse bursts greater than 10 Hertz.
13. Apparatus as claimed in Claim 6 wherein the laser light has a wavelength between 350 nanometers and 550 nanometers.

-21-

14. Apparatus adapted for use in breaking down material for removal from within a body characterized in that it comprises:

means for surrounding the material with liquid;

means for positioning the distal end of optical fiber against or very near to a localized region of the material; and

means for illuminating the localized region of the material with a pulsed laser through the optical fiber at a wavelength and with sufficient energy and intensity to cause in the operation of the apparatus a shockwave and to fragment the material beyond the localized region.

15. Apparatus as claimed in Claim 14 wherein the pulsed laser is arranged for a pulse duration of between .05 and 2 microseconds.

16. Apparatus as claimed in Claim 15 wherein the illuminating means is capable of delivering an intensity of the light at the localized region reaching the level of at least 5 megawatts per square centimeter.

17. Apparatus as claimed in Claim 15 wherein the pulsed laser is capable of delivering energy per pulse between 5 millijoules and 200 millijoules.

-22-

18. Apparatus as claimed in Claim 14, 15, 16 or 17 wherein the pulsed laser is a dye laser.
19. A method of breaking down material for removal from within a body comprising:
  - 05       surrounding the material with liquid; and
  - illuminating a localized region of the material with a pulsed laser at such wavelengths and with sufficient energy and intensity to cause fragmentation of the
  - 10       material without delivering energy sufficient to cause significant damage to other tissue in the vicinity of said material.
20. A method as claimed in Claim 19 wherein a shockwave is generated from the localized region to cause fragmentation of the material substantially beyond the localized region.
  - 15
21. A method as claimed in Claim 19 wherein the localized region is illuminated through optical fiber.
22. A method as claimed in Claim 21 wherein the distal end of the optical fiber is placed in contact with or very near to the localized region of the material.
  - 20
23. A method as claimed in Claim 19 wherein the pulsed laser is a dye laser.
  - 25



-23-

24. A method as claimed in Claim 19, 20, 21, 22 or 23 wherein the pulse duration of the pulse laser is between .05 microsecond and 2 microseconds.
- 05 25. A method as claimed in Claim 24 wherein the pulse duration is greater than .1 microsecond.
26. A method as claimed in Claim 24 wherein the intensity of the light at the localized region reaches the level of at least 5 megawatts per square centimeter.
- 10 27. A method as claimed in Claim 24 wherein the energy per pulse from the pulsed laser is between 5 millijoules and 200 millijoules.
- 15 28. A method as claimed in Claim 24 wherein the optical fiber has a diameter of between 60 microns and 600 microns.
- 20 29. A method as claimed in Claim 24 wherein pulse bursts from the pulsed laser are applied to the material to fragment the material and, thereafter, single pulses are applied to individual fragments to further break up the material.

-24-

30. A method as claimed in Claim 29 wherein the repetition rate of the pulse bursts is greater than 10 hertz.
- 05 31. A method as claimed in Claim 24 for fragmenting urinary calculi wherein the laser light has a wavelength between 350 nanometers and 550 nanometers.
- 10 32. A method of breaking down material for removal from within a body comprising:  
surrounding the material with liquid;  
positioning the distal end of optical fiber against or very near to a localized region of the material; and  
15 illuminating the localized region of the material with a pulsed laser through the optical fiber at a wavelength and with sufficient energy and intensity to cause a shockwave and to fragment the material beyond the localized region.
- 20 33. A method as claimed in Claim 32 wherein the pulse duration is between .05 microsecond and 2 microseconds.
- 25 34. A method as claimed in Claim 33 wherein the intensity of the light at the localized region reaches the level of at least 5 megawatts per square centimeter.

WO 86/06269

PCT/US86/00886

-25-

- 05 35. A method as claimed in Claim 33 wherein the energy per pulse from the pulsed laser is between 5 millijoules and 200 millijoules and the pulse duration is between .1 microsecond and 2 microseconds.
36. A method as claimed in Claim 33 wherein the optical fiber has a diameter between 60 microns and 600 microns.
- 10 37. A method as claimed in Claim 32, 33, 34, 35 or 36 wherein the pulsed laser is a dye laser.

# INTERNATIONAL SEARCH REPORT

International Application No PCT/US 86/00886

<b>I. CLASSIFICATION OF SUBJECT MATTER</b> (If several classification symbols apply, indicate all) *		
According to International Patent Classification (IPC) or to both National Classification and IPC		
IPC <sup>4</sup> : A 61 B 17/00		
<b>II. FIELDS SEARCHED</b>		
Minimum Documentation Searched *		
Classification System	Classification Symbols	
IPC <sup>4</sup>	A 61 B	
Documentation Searched other than Minimum Documentation to the extent that such Documents are included in the Fields Searched *		
<b>III. DOCUMENTS CONSIDERED TO BE RELEVANT</b> †		
Category *	Citation of Document, †† with indication, where appropriate, of the relevant passages ‡	Relevant to Claim No. ††
X, P	Biomedizinische Technik, vol. 30, no. 7/8, July/August 1985 (Berlin, DE) Schmidt-Kloiber et al.: "Laserinduced shock-wave lithotripsy (LISL)", pages 173-181, see abstract; page 174, left-hand column, lines 26-33	1-4, 6, 7, 14, 15, 18-22, 24, 25, 29, 31, 33
	--	
X	DE, A, 2412690 (SCHMIDT-KLOIBER) 17 October 1974 see page 5, line 12 - page 6, line 31	1, 2, 6-12, 14-17, 19, 20, 24, 25, 27-30, 33-36
	--	
X, P	WO, A, 85/03631 (WASHINGTON RESEARCH FOUND.) 29 August 1985 see abstract; page 14, lines 36-38; page 15, lines 1-20	1, 2, 6, 7, 9, 13, 15, 17, 19, 20, 24, 25, 27, 31, 33, 35
	--	./.
<p>* Special categories of cited documents: ††</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubt on priority claims or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance: the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance: the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art</p> <p>"A" document member of the same patent family</p>		
<b>IV. CERTIFICATION</b>		
Date of the Actual Completion of the International Search	Date of Mailing of this International Search Report	
12th August 1986	10 SEP 1986	
International Searching Authority	Signature of Authorized Officer	
EUROPEAN PATENT OFFICE	L. FOSSI	

III. DOCUMENTS CONSIDERED TO BE RELEVANT (CONTINUED FROM THE SECOND SHEET)		
Category *	Citation of Document, with indication, where appropriate, of the relevant passages	Relevant to Claim No
X	DE, A, 2538960 (DORNIER) 7 April 1977 see page 4, lines 4-21	1, 2, 6, 7, 9, 15, 17, 19, 20, 24, 25, 33, 35
	--	
X	US, A, 4207874 (CHOY) 17 June 1980 see abstract; column 3, lines 13-66	1, 3, 4, 5, 14, 18, 19, 21, 22, 23, 27
	--	
X, P	EP, A, 0153847 (SHILEY) 4 September 1985 see abstract; page 3, lines 2-26	1, 3, 4, 10, 14, 18, 19, 21, 22, 36
	--	
X, P	EP, A, 0152766 (SHILEY) 28 August 1985 see abstract; page 6, lines 24-28	1, 3, 4, 8, 14, 16, 18, 19, 21, 22, 27, 34
	--	
X, P	EP, A, 0144764 (IBM) 19 June 1985 see abstract; page 5, lines 6-13	1-4, 13, 14, 18- 22, 31
	--	
A	WO, A, 85/00510 (WEBSTER) 14 February 1985 see abstract	1, 3, 4, 14, 18, 19, 21, 22
	-----	

## ANNEX TO THE INTERNATIONAL SEARCH REPORT ON

INTERNATIONAL APPLICATION NO. PCT/US 86/00886 (SA 13345)

This Annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report. The members are as contained in the European Patent Office EDP file on 27/08/86

The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
DE-A- 2412690	17/10/74	AT-A,B 321448	25/03/75
WO-A- 8503631	29/08/85	EP-A- 0173717	12/03/86
DE-A- 2538960	07/04/77	None	
US-A- 4207874	17/06/80	GB-A,B 2017506	10/10/79
		JP-A- 54132381	15/10/79
		CA-A- 1105560	21/07/81
EP-A- 0153847	04/09/85	JP-A- 60176641	10/09/85
EP-A- 0152766	28/08/85	AU-A- 3799685	01/08/85
		DE-A- 3502331	01/08/85
EP-A- 0144764	19/06/85	AU-A- 3427684	13/06/85
		JP-A- 60126171	05/07/85
WO-A- 8500510	14/02/85	EP-A- 0150185	07/08/85
		US-A- 4576177	18/03/86

1 / 3

FIG. 1

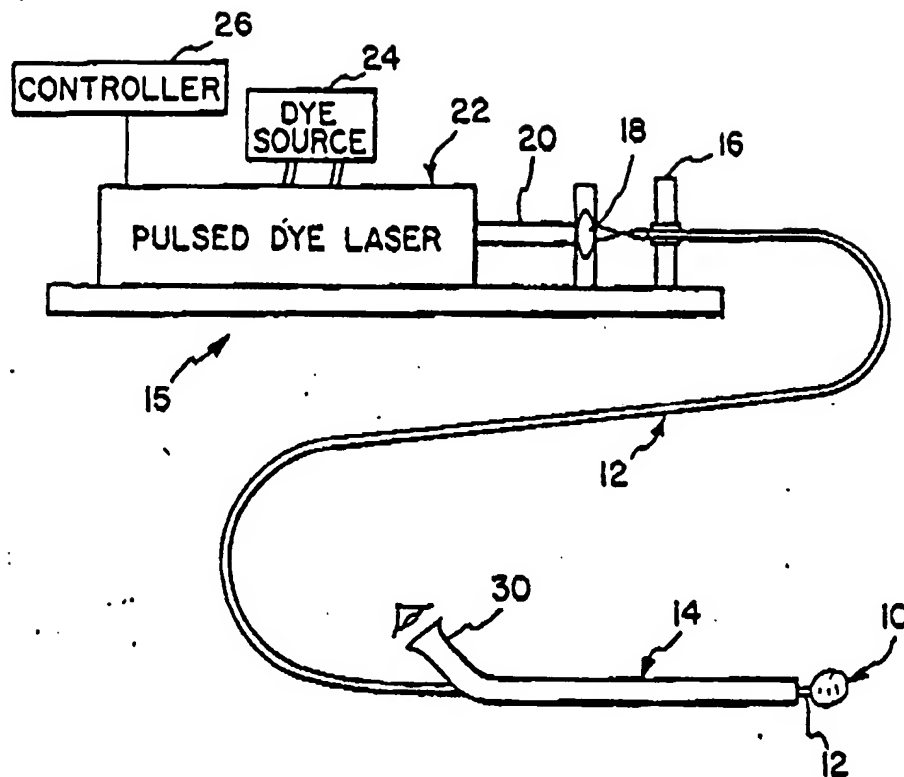
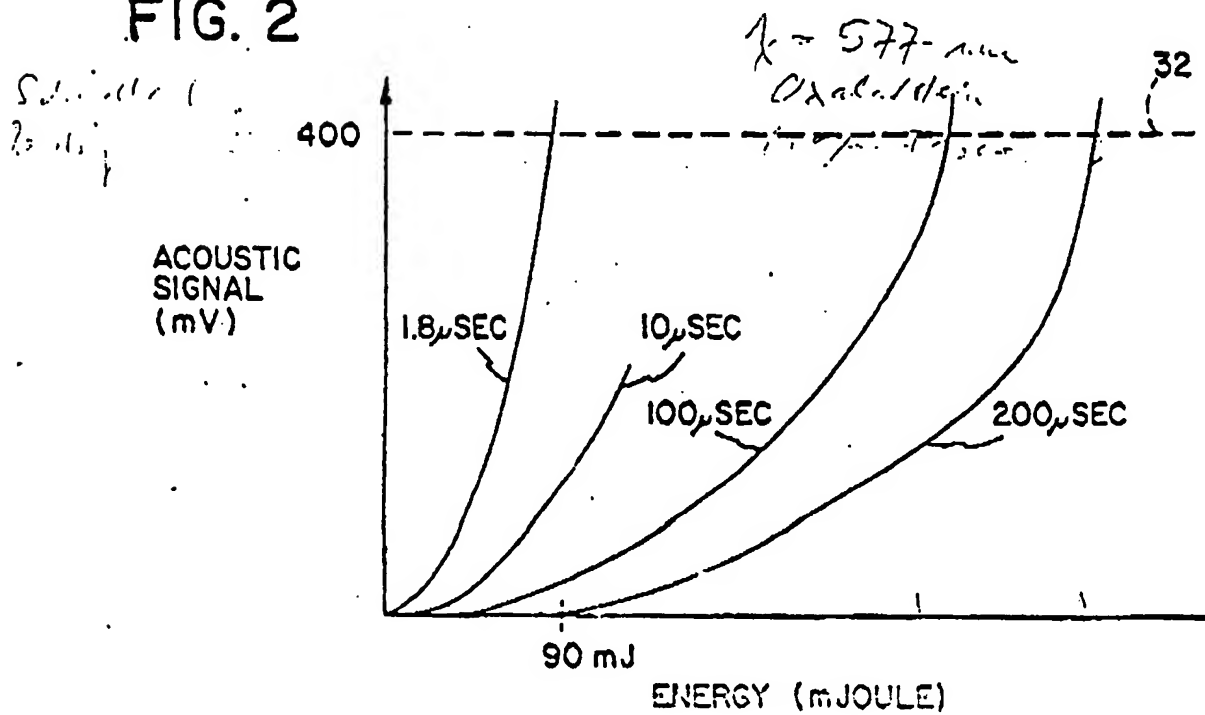


FIG. 2



2 / 3

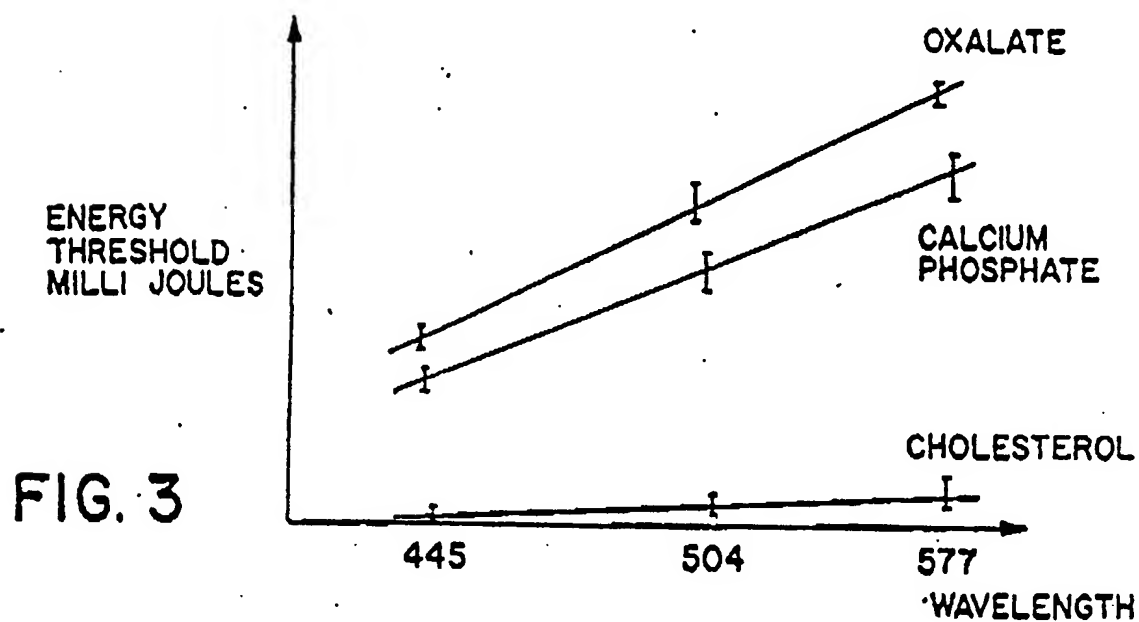
*aluminum fiber = 25 μm*

FIG. 3

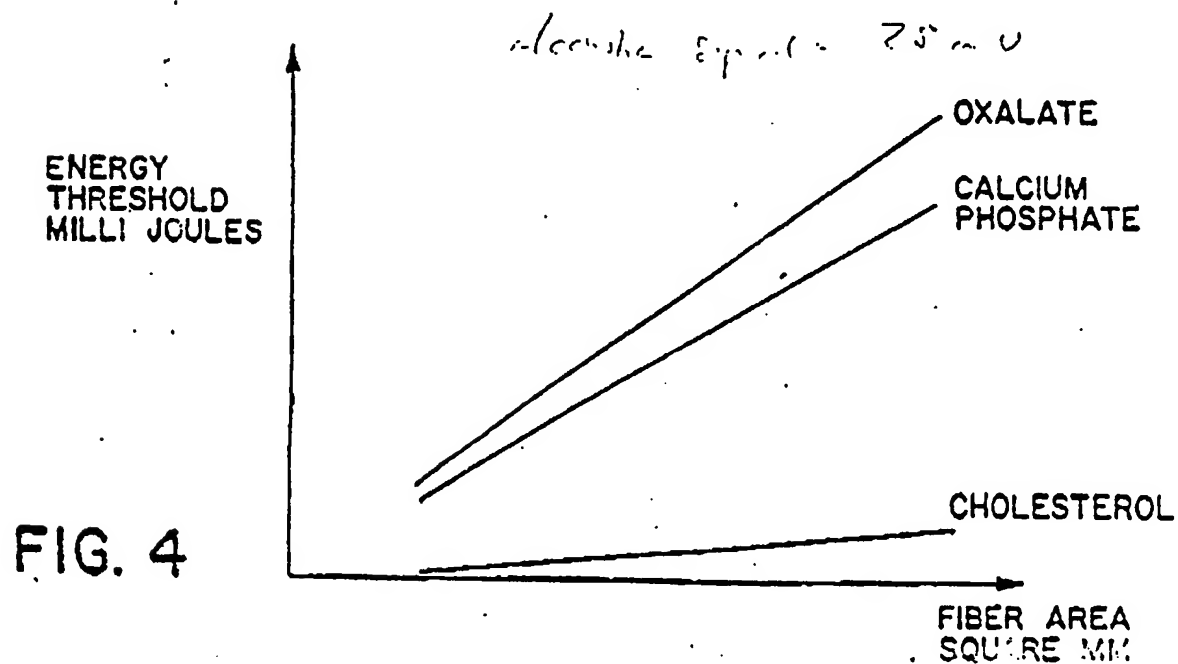


FIG. 4



8 / 3

FIG. 5

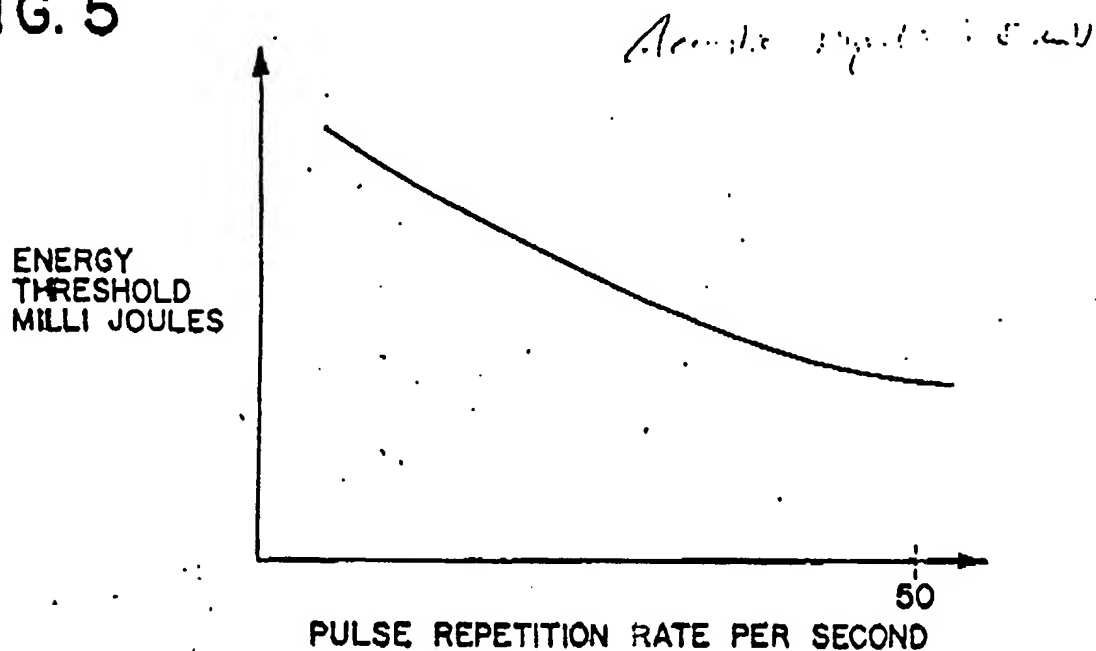
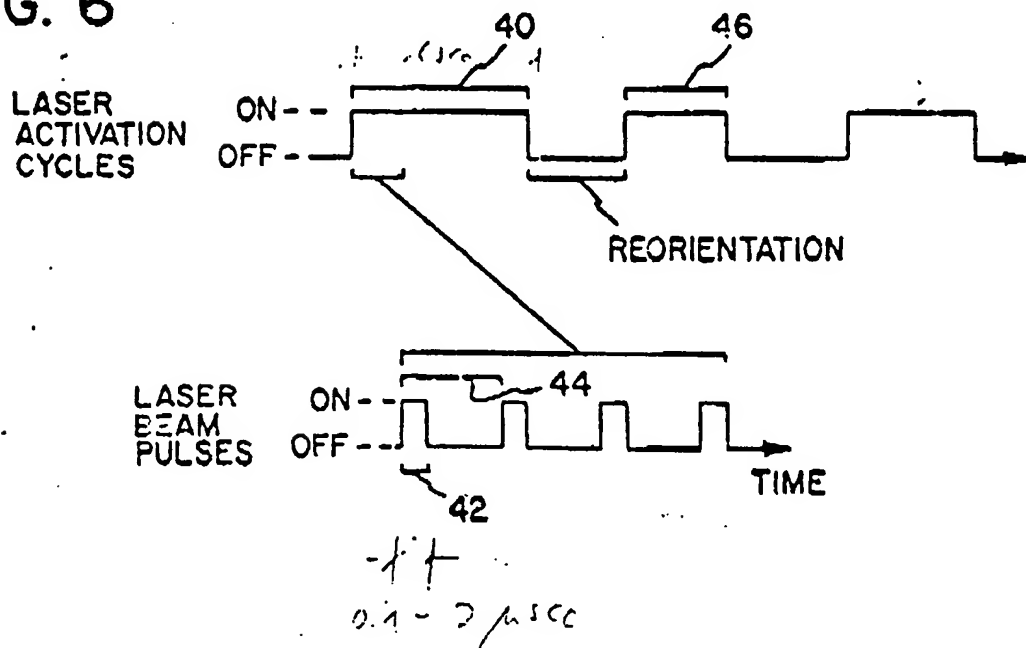


FIG. 6



**This Page is Inserted by IFW Indexing and Scanning  
Operations and is not part of the Official Record**

**BEST AVAILABLE IMAGES**

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images include but are not limited to the items checked:

- ☐ **BLACK BORDERS**
- ☐ **IMAGE CUT OFF AT TOP, BOTTOM OR SIDES**
- ☐ **FADED TEXT OR DRAWING**
- ☐ **BLURRED OR ILLEGIBLE TEXT OR DRAWING**
- ☐ **SKEWED/SLANTED IMAGES**
- ☐ **COLOR OR BLACK AND WHITE PHOTOGRAPHS**
- ☐ **GRAY SCALE DOCUMENTS**
- ☐ **LINES OR MARKS ON ORIGINAL DOCUMENT**
- ☒ **REFERENCE(S) OR EXHIBIT(S) SUBMITTED ARE POOR QUALITY**
- ☐ **OTHER:** \_\_\_\_\_

**IMAGES ARE BEST AVAILABLE COPY.**

**As rescanning these documents will not correct the image problems checked, please do not report these problems to the IFW Image Problem Mailbox.**